## 2. Resistive Strain strain Gauge gauge

Resistive potentiometers were described in the previous section, and they They measure involved displacement that was being measured by potentiometry but without altering the properties of the used resistance used. However In contrast, resistive strain gauges measure displacement with changes to a resistance that result result resulting from the transducer element being strained by a the displacement (National Instruments, 1998). A fractional change in length defines the strain (Figure 3; Equation 5), as shown in Figure 3.

Force H Force L  $\Delta L$ 

Figure 3. Definition of <u>Ss</u>train is <u>as a</u> fractional change in length (Adapted from National Instruments, 1998).

$$\varepsilon = \frac{\Delta L}{L}$$
(5)

There are various designs of resistive strain gauge designss (National Instruments, 1998). A piezoresistive strain gauge is a semiconductor device where the resistance varies nonlinearly **Commented [CP1]:** In the remainder of the text, the headings are in "sentence case," which is where only the first word and proper nouns are capitalized. I changed this heading to ensure a consistent style.

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with strain is called a piezoresistive strain gauge. The most commonly used design of <u>for a</u> resistive strain gauge is the bonded metallic strain gauge, <u>that which</u> consists of fine wire or metallic foil arranged in a grid pattern, <u>t.</u> This <u>design</u> maximizes the amount of metal subjected to parallel strain. Th<u>e</u>is grid is bonded onto a thin "carrier" backing, and <u>this the</u> carrier is attached to the <u>subject being measured measured subject</u>. So Therefore, any strain experienced by the test subject is transferred to the strain gauge, <u>this producinges</u> a <u>response of a linear change in</u> <u>electrical resistanclinear change in electrical resistance response</u>.

Gauge factor (GF) is a parameter which that expresses defines a strain gauge's sensitivity to strain. It means is expressed as the ratio of fractional change in electrical resistance to the fractional change in length (strain):

$$GF = \frac{\Delta R / R}{\Delta L / L} = \frac{\Delta R / R}{\varepsilon}$$
(6)

For metallic strain gauges, GF mostly has a value of -2 values are typically around approximately two.

Because <u>As</u> most strain measurements involve very small <u>quantities of strains</u>, and <u>the</u> GF is <u>approximately two-2</u>, <u>tiny small</u> changes in electrical resistance <u>are generally small</u> usually result (National Instruments, 1998). To measure these small resistance changes, you should use strain gauges in a bridge configuration with a voltage or current excitation sourceStrain gauges are used in a bridge configuration with a voltage or current excitation source **Commented [CP3]:** As a rule, numbers below 10 are spelled out unless the number is associated with a unit.

to measure these small resistance changes. A Wheatstone bridge (Figure 4) is composed consists of 4-four resistive arms plus with an excitation voltage ( $V_{ex}$ ) applied across the bridge.

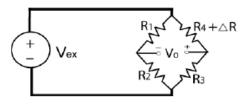


Figure 4. Wheatstone bridge (Adapted from National Instruments, 1998).

Output The output voltage of the bridge, V<sub>o</sub>, can be <u>calculated in using</u> Equation 7:

$$\boldsymbol{V}_{o} = \left[\frac{\boldsymbol{R}_{3}}{\boldsymbol{R}_{3} + \boldsymbol{R}_{4}} - \frac{\boldsymbol{R}_{2}}{\boldsymbol{R}_{1} + \boldsymbol{R}_{2}}\right] \cdot \boldsymbol{V}_{ex} \tag{7}$$

Drawbacks to strain Strain gauges suffer from several drawbacks, include including the facts that great precision is required during the manufacturing process, and that moisture effects can e reduce reduction in the long long-term reliability of measurements due to moisture effects unless the strain gauge is hermetically sealed (Measurements Group, 2001).

Strain gauges have a number of several benefits (Measurements Group, 2001)<sub>a</sub>. They are typically including their typically small size and have a low mass. They are also durable and

**Commented [CP4]:** I would suggest moving the drawbacks after the benefits to place more emphasis on the benefits of strain gauges.

**Commented [CP5]:** I combined these two paragraphs because they share a common focus (**highlighting the characteristics of strain gauges**). Paragraphs only need to be divided when you are describing different subjects.

Additionally, having the drawbacks and benefits in the same paragraph allows the reader to observe the contrasting features more directly. Ideas within a given paragraph are assumed to be connected, so your audience will already be in the mindset to connect these ideas. <u>shock-resistant due to have atheir</u> bonded construction and <u>a-lack of of moving parts</u>, and this makinges them durable and shock resistant. Linearity is great <u>excellent for over</u> a large wide range of strains, and their measurements are stable over time. Strain gauges are also fairly reasonably <u>cheap</u>inexpensive.

Omega Engineering, Inc. (Stamford, CT) offers many models of strain gauges which that have measurement ranges appropriate for human kinematic studies. These gauges are eheap <u>inexpensive</u> and long-lasting, with <u>a</u> fatigue limit exceeding <u>100000000 ten million</u> cycles (Omega Engineering Inc., 2007). Their SGD series of gauges <u>has have</u> a <u>gauge factor GF</u> of  $2.0 \pm$ 5%.

<u>Applications that sStrain gauges have been used to measure include-human movementss</u>, <u>such as Ss</u>houlder tension (Hughes et al., 1999) and ankle strain (Vandervoort et al., 1992) include the human movement applications that strain gauges have been used for.

3. Inductive displacement transducer

This Inductive type of displacement transducers type employs methods using uses methods using the inductance variation of inductance of single coils or the mutual inductance of two coils (Cobbold, 1974). The first type of methods are is based on inductance change in one coil either through a changes in the its geometry of the coil or in the properties of magnetic path properties. The second type of systems, which involves 2-two or more coils, uses a change in mutual coupling which resultings from relative coil displacement or from the movement of a coupling core movement.

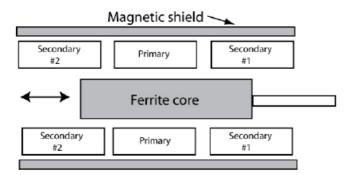
Among the various types of inductive displacement transducers,  $t_{\rm T}$  he linear variable differential transformer (LVDT) is one of among the most popular inductive displacement

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<u>transducer types</u> (Cobbold, 1974). One reason <u>that for</u> the LVDT<u>'s</u> is popularity is its large output for small movements. The LVDT is made up of consists of 3 coils: one primary coil and two <u>identical</u> secondary coils that are the same. It has a shifting core that can alter the coupling between the <u>3-three</u> coils, <u>this</u>-producing es the output displacement signal (Figure 5).



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Figure 5. Construction of <u>a</u> linear variable differential transformer (LVDT) Displacement is measured by <u>the It's</u>-movable core's interaction with the <u>3-three</u> coils <u>makes a measures of the displacement</u>. (Adapted from Cobbold, 1974.)

In general, vVoltages in the 1—10 V range are generally used, and commercial LVDT<sup>2</sup>s have sensitivities of approximately 0.5\_—2.0 mV\_per\_40.001 cm displacement per volt of excitation. The RDP Group (Pottstown, PA) makes their ACT LVDT Displacement Transducer, produced by the , this RDP Group (Pottstown, PA), featuringeses a measurement range up to ±470 mm, greatexcellent accuracy, sensitivity of 700 mV/V sensitivity, and infinite resolution (RDP Group: Menu of Displacement Transducers, 2007). Their ACT8000C model, which has a range of ±200 mm\_and , costs \$635 (Socie, 2007). LVDTs are many timesoften used in for

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physiological measurements of displacement, force, and pressure measurements (Cobbold, 1974).

## 4. Capacitive displacement transducer

Capacitive displacement transducers function by the factor the principle that a change in capacitance is proportional to the change in displacement of the object that is being measured (Norton, 1989). Displacement is able tocan be converted to an electrical output using the capacitor plate separation distance<sub>35</sub> the plate area dependence<sub>3</sub> of capacitance on plate area and the permittivity of the medium between the capacitor plates (Cobbold, 1974). While it is an issue that all capacitive transducers face the problem have the disadvantage that displacement makes causes relatively small changes in capacitance, by the use of particular using specialized circuit techniques allows these transducers can to have results in great excellent accuracies and sensitivities  $\leq 0$  for  $10^{-12}^{-12}$  cm or better (Sydenham, 1972).

If we ignore the effects of electrical field fringing at <u>the plate edges are ignored</u>, capacitance is given by Equation 8:

$$C = \frac{\varepsilon A}{d} \quad (\text{in Farads}) \tag{8}$$

where A is <u>the plate area</u> (in cm<sup>2</sup><sup>2</sup>), d is <u>the plate separation</u> (in cm), and  $\varepsilon$  (in F/cm) is the <u>mediums</u> permittivity <u>of the medium</u> separating the plates.

A basic capacitive displacement transducer is <u>shown</u> in Figure 6, <u>where C</u> represents a capacit<u>orive</u> plate, and x is the distance between plates:

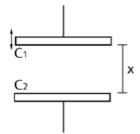


Figure 6. Basic design of <u>a capacitative capacitive</u> displacement transducer. (Adapted from Cobbold, 1974.)

The <u>direct current</u> (DC) polarizing circuit is shown in Figure 7 and it is one of the simplest circuits that is able to can respond proportionally to the displacement of such a parallel-plate capacitor transducers (:Figure 7).

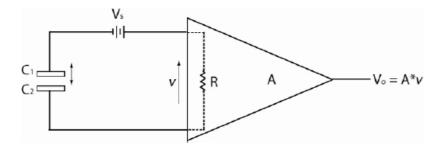


Figure 7. DC-polarized <u>capacitative\_capacitive</u> displacement transducer.  $V_s$  is <u>the</u> voltage source, C represents a capacitor plate, R is resistance, v is <u>the</u> voltage across the resistance, A is <u>the</u> ampilfier amplifier gain, and  $V_o$  is <u>the</u> output voltage. (Adapted from Cobbold 1974.)

For this system, the output voltage v is given by Equation 9:

$$v = \frac{VC_0 R}{d} \left( \frac{j\omega}{1 + j\omega C_0 R} \right) x_0 e^{j\omega t}$$
(9)

Wwhere d is the plate separation distance,  $x_{\underline{00}}$  is the sinusoidal plate displacement

aplitude amplitude,  $C_{\underline{0}} = (\varepsilon A)/d$ , and V is the DC-polarization voltage. If  $\omega C_{\underline{0}} R >> 1$ , Equation

9 becomes:

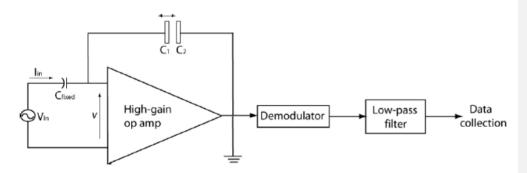
$$v = \frac{V x_0 \sin \omega t}{d} \tag{10}$$

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By iInspection of Equations 9 and Equation 10, we see that at indicates that higher frequencies the system's response is proportional to the inverse displacement at higher frequencies. hHowever-, for the response is reduced at lower frequencies lower frequencies the response is reduced, and becomes 0-zero if when  $\omega = 0$ . This system'se lack of DC response of this system is a concerning when measuring many physiological quantities.

To solve t<u>This</u> problem can be solved by using <u>, a we should use the transducer as the feedback</u> component of a high-gain operational amplifier<u>, since The transducer transforms</u> the problematic inverse displacement\_-vs.\_-capacitance relation <u>now-to becomes a simpler</u> linear output voltage\_-vs.\_-displacement relation that we can work with. The circuit diagram of this such a <u>different</u>-system is shown in Figure 8<del>;</del>.



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Figure 8. <u>System diagram Diagram of a linear displacement measurement system using</u> <u>eapacitative\_capacitive</u> sensing. (Adapted from Cobbold, 1974.)

<u>As an exampleOne such linear displacement measurement system</u>, the Sensagap capacitive displacement sensor, <u>from the RDP Group</u> can be <u>acquired used for kinematic measurements in</u>

<u>over</u> a variety of measurement ranges that are able to be used for kinematic measurements. It, features <u>a</u> linearity of  $\pm 0.5\%$  <u>of</u> full-scale or better and can withstand shocks up to 20\_g (RDP Group: Sensagap Capacitive Displacement Transducer, 2007).

References:

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RDP Group, Sensagap Capacitive Displacement Transducer. 2007. http://www.rdpe.com/us/sg.htm

Vandervoort AA, Chesworth BM, Cunningham DA, Rechnitzer PA, Paterson DH, Koval JJ<del>,</del> An Outcome Measure to Quantify Passive Stiffness of the <u>aA</u>nkle. *Can J Public Health*, Jul\_-Aug<sub>7</sub> 83, Suppl 2: S19–23, 1992.

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